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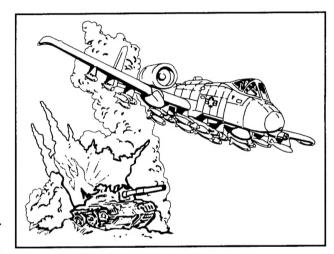
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- 13. Abstract: This forecaster memo describes a process designed to improve the bombing accuracy of A-10 aircraft equipped with the Low Altitude Safety and Targeting Enhancement (LASTE) system by improving altimeter setting accuracy. After finding unacceptable altitude errors during tests of LASTE Version 3.3. The 57th Test Group (57 TG) at Nellis AFB asked the 57 OSS/OSW to develop a method for improving A-10 bombing accuracy by developing improved altimeter setting forecasts. The 57 TG also contracted for General Electric to include software in LASTE Version 4 to correct for these altitude errors automatically. This memo describes a method for improving altimeter setting forecasts in support of LASTE Version 3.3. It also explains basic altimetry theory and tells how the theory relates to the A-10 bombing problem. Finally, the memo provides weather forecasting tips for supporting the new LASTE Version 4.
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PREFACE

This forecaster memo describes a process designed to improve the bombing accuracy of A-10 aircraft equipped with the Low Altitude Safety and Targeting Enhancement (LASTE) systems by improving altimeter setting accuracy. The 57th Test Group (57 TG) at Nellis AFB asked the 57 OSS/OSW to develop a method for improving A-10 bombing accuracy through corrected altimeter settings after finding unacceptable altitude errors during tests of LASTE Version 3.3. The 57 TG also contracted with General Electric to develop software (LASTE Version 4) to correct for these altitude errors automatically. This memo discusses a method for improving altimeter settings for LASTE Version 3.3. It also explains basic altimetry theory and tells how the theory relates to the A-10 bombing problem. Finally, the memo provides weather forecasting tips for supporting the new LASTE Version 4.

For a pilot's perspective on altimeter settings and more detail on the LASTE 3.3 and 4.0, read "Reaching New Heights with LASTE" in the Summer 1993 Weapons Review.

The author owes thanks to several people. The basic idea for using altimeter settings to correct for the A-10 altitude errors was worked out in conversations with Mr. Al Caudel. MSgt Wayne Bradshaw provided valuable comments on the development of the manual method for forecasting LASTE 3.3 altimeter settings. The 57 OSS/OSW



forecasters tested these methods and provided feedback to improve the process. Finally, Maj Dan Brees, Lt Col Frank Estis, Dr. Dale Meyer, and Lt Col James Davenport helped edit this memo to make it understandable.

INTRODUCTION

To put bombs on target, A-10 aircrews need accurate altitude measurements. During testing of the Low Altitude Safety and Targeting Enhancement (LASTE) 3.3 system, A-10 pilots found differences as large as 400 feet between barometric altimeter readings and those indicated by the radar altimeter. When A-10 pilots asked us for help, we developed a simple method for providing altimeter setting forecasts to be entered into the LASTE 3.3 system.

The 57th Test Group at Nellis also contracted with General Electric to develop an automated model for the next LASTE version (LASTE 4), with the improved altimeter settings built-in. The new version should work well under most environmental conditions, but with several limitations that are explained in this memo. The 57th Test Group is testing LASTE 4 now; operational A-10 units should transition to the new equipment in 1994 or 1995. In the meantime, forecasters can use the correction method described next to support A-10s using the LASTE 3.3 system.

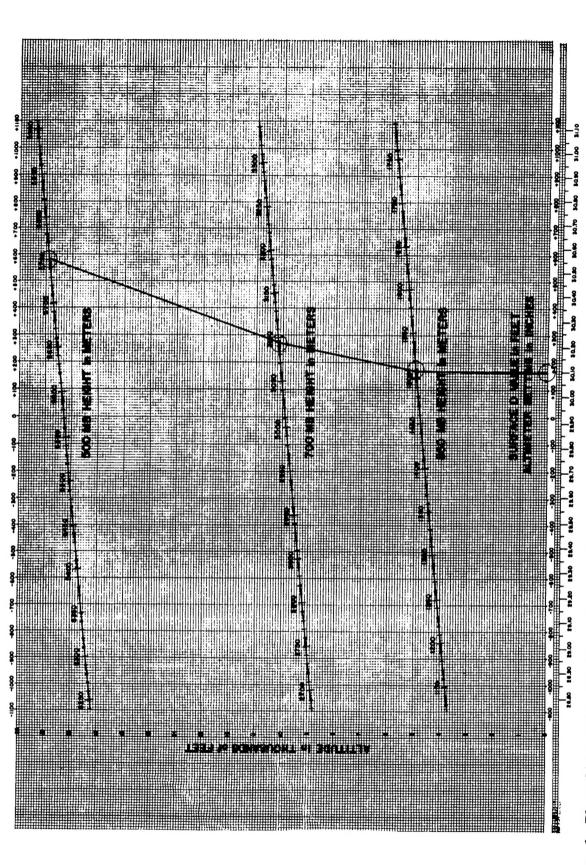
This next section tells you how to compute LASTE 3.3 altimeter setting forecasts by using forecast heights of pressure surfaces. If your only interest is in getting the immediate job done, read no further. But if you'd like a refresher on altimetry and how it relates to dropping bombs from A-10s, read on. The last part of the memo describes certain weather limitations in the new LASTE 4 and offers tips to forecasters who will support it.

ALTIMETER SETTING FORECASTS FOR LASTE 3.3

Success in forecasting altimeter settings depends on forecasting the heights of constant pressure surfaces accurately. It is important to use *forecast* pressure surface heights (rather than observed values) to keep the accuracy within reasonable limits. If the model you are using does not include this information, you may want to consider factoring in the average diurnal variation of the height of the pressure levels by developing a table of diurnal variations for each month of the year You can then compute the forecast altimeter settings using the following procedure:

- Compute forecast sea-level pressure and heights of the 850, 700 and 500 millibar (mb) pressure levels for the target location and time over target.
- Plot the sea-level pressure, in inches of mercury, at zero feet above mean sea level (MSL) on a D-Value Computation Chart (AF Visual Aid 105-35).
- Plot the forecast heights, in meters, for the pressure levels on the chart. Connect the points to interpolate the values to MSL altitudes.
- Follow the constant D-Value line for each bombing altitude straight down to the bottom of the chart. The altimeter setting at the bottom of the chart is the correct altimeter setting for this altitude.

Figure 1 (Next page) is a plotted example.



of the pressure levels are 1,510, 3,090, and 5,750 meters for 850, 700 and 500 mb, respectively. In this example, the altimeter setting for 5,000 feet MSL is 30.11 inches; for 10,000 feet, 30.22 inches; and for 15,000 feet, 30.45 inches. The Figure 1. Plotted Example on D-Value Computation Chart (AFVA 105-35). Sea-level pressure is 30.10 inches. The heights error would be over 300 feet in altitude if you used the altimeter setting for 5,000 feet at 15,000 feet.

The method described here is not new. Weather forecasters use it routinely to determine D-Values. We've just taken it a step farther to provide pilots with altimeter settings equivalent to the D-Value. Since pilots understand altimeter setting better than D-Value, they can better include the new method in the flight planning process. There can be a problem when the altimeter setting is higher than 31.00 inches since this is the maximum value in the aircraft altimeter's Kohlman window. We have not experienced this problem during testing at Nellis AFB, but it could occur at other locations.

We've also developed a computer program to calculate the improved altimeter setting. The inputs to the program include sealevel pressure and the forecast heights of the 1,000-mb and 925-mb levels, as well as those for 850 mb, 700 mb, and 500 mb. The results are the same for the computer or the manual method.

ALTIMETRY THEORY

What follows is a short refresher on altimetry. After that, we'll explain how theory relates to insuring accurate bomb release altitudes.

To understand how an aircraft altimeter works, we first need to understand how pressure changes with height in a constant lapse rate atmosphere. When working with the atmosphere, we assume that air is an ideal gas and that the pressure change with a change in altitude depends only on air density and gravity. The two equations describing these assumptions are the *ideal gas law* and the *hydrostatic equation*. Water vapor in the atmosphere causes problems when using the ideal gas law. In order to determine the correct air density

of an air parcel with water vapor, we need to use *virtual temperature* rather than dryair temperature; virtual temperature is the temperature a dry-air parcel would have if its density and pressure equaled the density and pressure of the parcel with water vapor. Virtual temperature is always higher than dry-air temperature because water vapor is less dense than dry air.

Using the ideal gas law and the hydrostatic equation, you can derive an equation relating the pressure to altitude under certain conditions (Hess, 1979, page 80). If we assume the lapse rate in the atmosphere to be constant, then this equation is:

$$p(z) = p(0)*(1 - \frac{\Gamma}{T_0}*z)^{\frac{g}{R*\Gamma}}$$
 Equation 1

p(0) and T_o are the sea-level pressure and sea-level virtual temperature, p(z) is the pressure at altitude z, and Γ is the virtual temperature lapse rate. The constants g and R are the gravitational acceleration (9.81 ms⁻²) and the gas constant for dry air (287 Joules K⁻¹ kg⁻¹).

The U. S. Standard Atmosphere assumes sea level pressure to be 1013.25 mb (29.92 inches), the surface temperature to be 15° C, the lapse rate to be 6.5° C per kilometer, and dry air (i.e., no water vapor). Using these constants and converting to measure altitude in feet, T/T_0 equals $6.875*10^{-6}$ ft⁻¹ and g/(R* Γ) equals 5.2561 in Equation 1.

Table 1 (next page) shows the U. S. Standard Atmosphere's relationship between altitude, pressure, and temperature calculated using Equation 1. An aircraft barometric altimeter simply converts a pressure measurement to an altitude, using

a barometer calibrated to match the U. S. Standard Atmosphere. By adjusting the aircraft altimeter's sea-level pressure,

p(0), the pilot corrects the pressure-altitude scale for deviations from the Standard Atmosphere.

Table 1. U.S. Standard Atmosphere Pressure and Temperature.

	PD FOOTIDE	TEMPERATURE
HEIGHT	PRESSURE	
(FEET)	(MB)	(O CELSIUS)
0	1013.25	15
1000	977	13
2000	942	, 11
3000ء	908	9
4000	875	7
5000	843	5
6000	812	3
7000 -	781	1
8000	752	-1
9000	724	-3
10000	697	-5
15000	572	-15
20000	466	-25
25000	376	-34
30000	301	-44

As you can see from the preceding discussion the three causes of deviation atmosphere are from the standard sea-level pressures, non-standard non-standard temperatures and lapse rates, and water vapor in the atmosphere. Each of these conditions affects the aircraft altimeter differently. A non-standard sea level pressure "slides" the standard atmosphere pressure scale up or down, depending on whether the sea level pressure is higher or lower than standard, respectively. D-Values are positive when the pressure is higher than standard, and negative when the pressure is lower than standard. Figure 2 (opposite) shows this effect for sea level pressures of 29.38, 29.92, and 30.42 inches.

Non-standard temperatures "stretch" or "shrink" the standard atmosphere. If the atmosphere is warmer than standard, the pressure change with a change in altitude is less than in the Standard Atmosphere; positive D-Values increase with height. If the atmosphere is colder than standard, the pressure change with a change in altitude Standard greater than in the Atmosphere; negative D-Values increase with height. A less than standard lapse rate (such as through an inversion) causes temperature to increase with height and has the same effect as warmer than standard temperatures. A greater than standard lapse rate has the same effect as temperatures that are colder than standard. Figure 3 shows the effects of cold and warm air masses.

Finally, humidity causes the atmosphere's density to decrease. This is equivalent to raising the temperature. Humidity, therefore, always acts to stretch the atmosphere. This effect explains why we

use the virtual temperature to determine the thickness value between two pressure levels rather than just the dry bulb temperature.

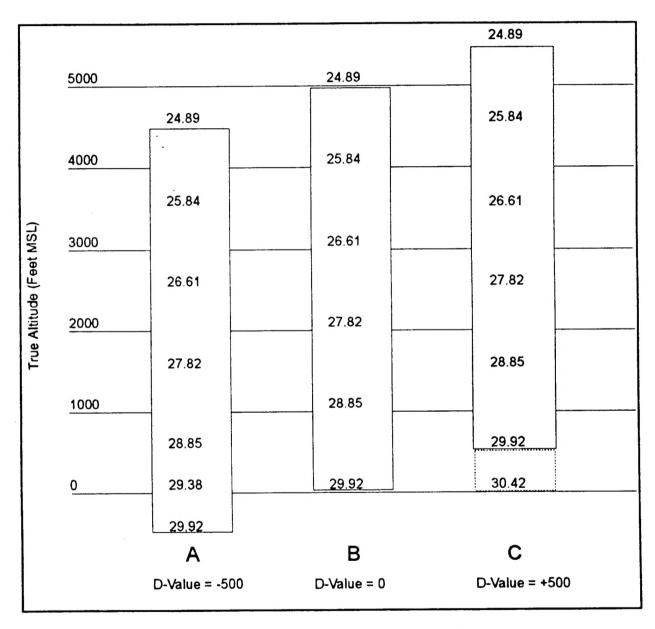


Figure 2. The Effects of Varying the Surface Pressure. All three atmospheres have standard lapse rates and the temperatures at 29.92 inches Hg are 15° C. Several common pressure levels are plotted at the appropriate height in each atmosphere.

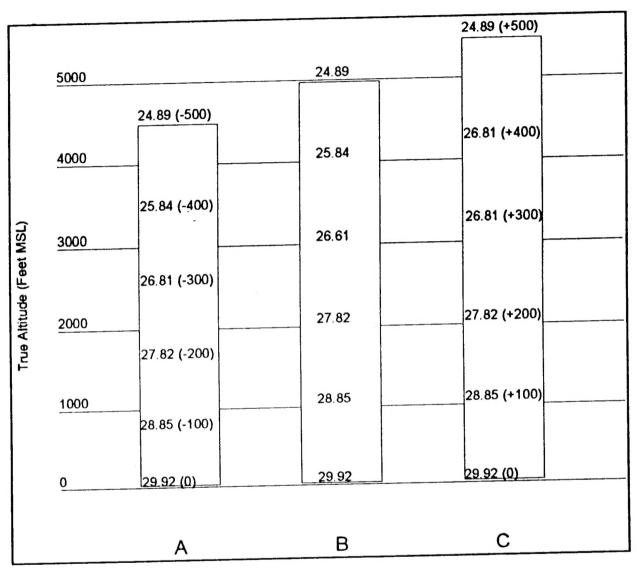


Figure 3. The Effects of Non-Standard Temperatures. All three atmospheres have the same sea level pressure. Atmosphere A is 10% colder than standard. Atmosphere B is the Standard Atmosphere. Atmosphere C is 10% warmer than standard. Several common pressure levels are plotted at the appropriate height in each atmosphere. The D-value associated with each pressure level is shown in the parenthesis next to the pressure value.

ALTIMETRY AND THE A-10 BOMBING PROBLEM

You may have wondered why, if LASTE uses a radar altimeter, A-10 pilots need improved altimeter setting forecasts. First, the radar altimeter only works below 5,000 feet AGL. Second, the radar altimeter needs fairly level terrain around the target to get an accurate reading. If it is safer to bomb from above the 5,000-foot range of the radar altimeter, or if the radar can't provide an accurate reading for whatever reason, the pilot will choose to bomb on the barometric altimeter.

The atmosphere above any given location is usually non-standard due to all three effects. The altimeter setting provided by the weather station only gives the aircrew an accurate altitude indication at *field elevation*; it is not necessarily accurate at other altitudes. We can, however, provide a more accurate altimeter setting for the release altitude by compensating for all the atmospheric effects that induce error.

The method we developed provides forecast altimeter settings for the weapon's release altitude. First, we rewrite Equation 1 to solve for sea- level pressure and substitute the U. S. Standard Atmosphere constants. The result is Equation 2.

$$p(0) = \frac{p(z)}{(1 - 6.875 * 10^{-6} ft^{-1} * z)^{5.2561}}$$
 Equation 2

Next, we forecast a pressure level (p(z)) to be at height z and use Equation 2 to calculate the altimeter setting (p(0)) that places the pressure level at this altitude. It is easiest to do this for the sea level pressure and the standard pressure levels. Finally, we interpolate between the altimeter settings from the nearest two standard pressure levels to determine the

altimeter setting for the release altitude. The D-Value chart does this graphically while a computer program solves the problem numerically.

In the past, we used the D-Value or altitude variation to describe (to aircrews) the deviation from the Standard Atmosphere. But the A-10 crews we worked with prefer the altimeter setting correction because it's easier to implement in flight planning.

HOW THE NEW LASTE 4 WORKS

As mentioned earlier, the 57th Test Wing is testing a new LASTE 4 version that uses instantaneous measurements temperature and pressure at flight level to provide a corrected altitude. LASTE Version 4 uses a known altitude (MSL) as a reference level for calculating the aircraft's instantaneous altitude. LASTE determines aircraft altitude at the reference level by using either the field elevation in the BARO mode or the radar altimeter in DELTA mode. The computer stores the airfield elevation and pressure altitude at field elevation for the BARO reference level during the takeoff roll. In DELTA mode, the pilot picks a location with fairly flat terrain and a known elevation, then takes a radar altimeter measurement and stores the aircraft altitude (feet AGL) in the aircraft computer. LASTE 4 then adds the terrain elevation (MSL) to the aircraft's altitude above the terrain to calculate the reference level height (MSL).

When LASTE 4 measures the radar altitude or the reference level, it also measures the pressure altitude at the DELTA reference level and stores it in computer memory for altitude calculations. As the aircraft changes altitudes, LASTE

4 continues to measure pressure altitude and temperature. The computer determines the aircraft's altitude at any given moment by adding a corrected altitude change to either the field elevation (BARO mode) or the reference level height (DELTA mode), depending on the mode the pilot chooses to use.

The LASTE 4 altitude correction depends on the pressure altitude at the reference altitude, as well as on the instantaneous pressure altitude and temperature measurements. LASTE 4 first subtracts the

pressure altitude at the reference level from the instantaneous pressure altitude measurement to determine the pressure LASTE altitude change (ΔPA) . multiplies the pressure altitude change by the ratio of the instantaneous temperature atmosphere (T_{me}) the standard temperature (T_{std}) for the instantaneous pressure altitude. LASTE 4 then adds the corrected altitude change to the reference height to determine the instantaneous computer The LASTE altitude. algorithm, then, becomes:

Instantaneous_Altitude = Reference_Altitude +
$$\Delta PA \times \frac{T_{true}}{T_{red}}$$
 Equation 3

Consider the following example. On takeoff, the aircraft is at a field elevation of 2,000 feet MSL; pressure altitude is 2,100 feet. The aircraft climbs to a new altitude and takes a DELTA reference above a terrain elevation of 3,000 feet. If the radar altimeter reads 3,000 feet AGL, then the DELTA reference height is 6,000 feet MSL. Let's assume that the pressure altitude measured at the

the DELTA reference level is 6,250 feet. Upon climbing to a new altitude, the LASTE measures a pressure altitude of 9,000 feet and a temperature of 283K. The standard atmosphere temperature at a pressure altitude of 9,000 feet is 270K (See Table 1). Therefore, the instantaneous altitude determined by the DELTA mode is:

Instantaneous_Altitude =
$$6000' + (9000'-6250') \times \frac{283K}{270K} = 6000' + 2000' \times 1.048$$
 Equation 4 = $6000' + 2882'$ = $8882'$

The BARO mode also continuously calculates an altitude. Table 2 shows the comparison of the BARO and DELTA calculations for the example described

above. The altitude displayed in the Heads Up Display and used for ballistics calculations depends on the mode chosen by the pilot.

Table 2. Comparison of BARO and DELTA Altitude Calculations.

Mode	Reference Altitude	PA at Reference	PA at Altitude	Change in PA	Ttrue	Tstd	Temp Ratio	Instantaneous Altitude
		2100	9000	6900	283	270	1.048	9232'
BARO	2000		9000	2750	283	270	1.048	8882'
DELTA	6000	6250	3000	1 2120				

We need to understand the hypsometric equation and thickness calculations to understand the LASTE 4 algorithm. The hypsometric equation (Equation 5) states that change in height ("thickness", ΔZ)

between one pressure level (p_0) and another pressure level (p) is proportional to the average virtual temperature $(T_{average})$ of the layer. R is the gas constant for dry air.

$$\Delta Z = R \times T_{average} \times \ln(\frac{p}{p_0})$$

Equation 5

In the standard atmosphere, the actual height of a pressure level equals the pressure altitude. Therefore, the thickness of a layer between two pressure levels in the standard atmosphere (Δz_{std}) equals the pressure altitude change (ΔPA). Also, the average virtual temperature ($T_{average}$) is

the average of the standard atmosphere temperatures $(T_{average_std})$ since the Standard Atmosphere assumes the atmosphere is dry. In this case, the temperature equals the virtual temperature. The LASTE calculation of the actual change in altitude becomes:

$$\Delta Z = \Delta PA \times \frac{T_{true}}{T_{true}} = \Delta Z_{std} \times \frac{T_{true}}{T_{etd}} = R \times T_{average_std} \times \ln(\frac{p}{p_0}) \times \frac{T_{true}}{T_{std}}$$
 Equation 6

The comparison of Equation 6 with Equation 5 shows that LASTE 4 approximates the average virtual temperature of the layer. LASTE multiplies the layer's average standard atmosphere temperature by the instant-

aneous temperature and divides the result by the standard atmosphere temperature for the instantaneous pressure altitude to determine the layer's average virtual temperature (Equation 7).

$$T_{average} = T_{average_std} \times \frac{T_{true}}{T_{std}}$$

Equation 7

LASTE 4 LIMITATIONS

The new software has some limitations that forecasters should know about. For example, Equation 7 represents an assumption made by the LASTE engineers about atmospheric temperatures that may not always be true. LASTE 4 can run into trouble under certain weather conditions, such as non-standard lapse rates. The hypsometric equation states that thickness depends on the mean virtual temperature of the laver. However, as shown in Equation 7, LASTE 4 uses one observed temperature reading to determine the layer average. Therefore, altitude errors may increase when the environmental lapse rate is non-linear or non-standard. possible problem lies in the fact that since LASTE 4 measures temperature (rather than virtual temperature), errors increase in high humidity environments; these errors, however, should not exceed 1 or 2 percent. Finally, LASTE 4 errors may increase as the aircraft moves away from the reference location; the height of the reference pressure altitude may change in time and space.

Pilot should know that inversions reduce BARO mode accuracy. To decrease the effects of non-standard lapse rates, be sure to brief LASE 4 aircrews on *inversion heights*, since they'll want to take their reference measurements either above or below the inversion depending on the bombing altitude. Remind pilots that the trapped smog and dust below the top of the inversion layer provides a good visual clue to the inversion height for the DELTA reference altitude. Also brief the dissipation time of a surface radiation inversion.

Pilots should take the DELTA reference as close to the target as possible so as to reduce the error due to the change in height of the reference pressure level. If this is not possible, we developed a technique to decrease errors due to this effect.

LASTE 4 provides pilots the option to manually enter a DELTA value for a specified altitude. The 57 TG and the 57 OSS/OSW use this option to allow the pilot to manually enter a forecast DELTA value into the LASTE 4 computer to correct for the change in height of the reference level. Since the LASTE 4 DELTA value is the instantaneous pressure altitude minus the aircraft altitude, the DELTA value equals the negative of the D-Value for the DELTA reference altitude (MSL). Therefore, the process for providing the aircrew a forecast DELTA value is:

- The pilot provides the weather station with the target location, the time over target, and the desired altitude (MSL) for the DELTA value.
- The weather forecaster determines D-Values for the target location using a D-Value computation chart, computer program, or other method.
- The weather forecaster provides the pilot with the negative of the D-Value for the desired altitude. As an example, use the situation described in Figure 1; the desired DELTA altitude is 8,000 feet, The D-Value at 8,000 feet is +210 feet and the resulting DELTA value is -210.

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107 WEATHER FLIGHT 26000 SOUTH ST BLDG 1516 SELFRIDGE ANGB MI 48045-5024	1
110 WEATHER FLIGHT HO 131 TEW. 10800 NATURAL BRIDGE RD BRIDGETON MO 63044-2371	1
111 WEATHER FLIGHT 14657 SNEIDER STREET ELLINGTON ANGB TX 77034-5586	1
113 WEATHER FLIGHT 824 E VANATTI CIRCLE TERRE HAUTE IN 47830-5012	1
116 WEATHER FLIGHT 307 6TH STREET MCCHORD AFB WA 98439-1201	1
120 WEATHER FLIGHT 19089 BRECKENBRIDGE AVE AURORA CO 80011-9527	1
120 WEATHER FLIGHT 19089 BRECKENBRILGE AVE AURORA CO 80011-9327	1
121 COS OTW BLDG 500 RICKENBACKER ANGB OH 43217-5005	
121 WEATHER FLIGHT 3252 E PERIMETER ROAD ANDREWS AFB MD 20331-5011	1
122 WEATHER FLIGHT 400 RUSSELL AVENUE NEW ORLEANS NAS LA 70143-5200	1
123 WEATHER FLIGHT 6801 CORNECOT ROAD PORTLAND OR 97218-2797	1
125 WEATHER FLIGHT 4200 N 93RD AVENUE TULSA OK 74115-1699	1
126 WEATHER FLIGHT 1919 EAST GRANGE AVE MILWAUKEE WI 53207-6298	1
127 WEATHER FLIGHT P.O. BOX 19061 FORBES ANGB TOPEKA KS 66619-5000	1
131 WEATHER FLIGHT 1 TANK DESTROYER BLVD BOX 35 BARNES ANGB MA 01085-1385	1
131 WEATHER FLIGHT I TANK DESTROYER BLVD BOX 33 BARNES ANGB MA 01003-1303	1
140 WEATHER FLIGHT (PAANG) 201 FAIRCHILD STREET WILLOW GROVE ARS PA 19090-5320	1
146 WEATHER FLIGHT 300 TANKER ROAD #4254 PITTSBURG IAP CORAOPOLIS PA 15108-4254	1
154 WEATHER FLIGHT CAMP ROBINSON NORTH LITTLE ROCK AR 72118-2200	
156 WEATHER FLIGHT 5225 MORRIS FIFLD DRIVE CHARLOTTE NC 28208-5797	1
150 MEATIED ELICIT DT 1 DOV 465 CAMP BLANDING STARKE EL 32091-9703	1
164 WEATHER FLIGHT RICKENBACKER IAP 7556 SOUTH PERIMETER ROAD COLUMBUS OH 43217-5910	1
165 WEATHER FLIGHT 1019 OLD GRADE LANE LOUISVILLE KY 40213-2678	1
169 FG SW WEATHER STOP 6 MCENTIRE ANGB, 1325 SOUTH CAROLINA RD EASTOVER SC 29044-5006	1
169 FG SW WEATHER STOP 6 MCENTIRE ANGB, 1325 SOUTH CAROLINA RD EASTOVER SC 25047-3000	
181 WEATHER FLIGHT 8150 W JEFFERSON BLVD DALLAS TX 75211-9570	1
195 WEATHER FLIGHT 106 MULCAHEY DRIVE BLDG 106 PORT HUENEME CA 93041-4003	
199 WEATHER FLIGHT 1102 WRIGHT AVENUE WHEELER AAF HI 96854-5200	1
200 WEATHER FLIGHT 5680 BEULAH RD. SANDSTON VA 23150-6109	1
202 WEATHER FLIGHT REDG 3138 OTIS ANGR MA 02542-5001	1
203 WEATHER FLIGHT 125 PINEGROVE ST FT INDIANTOWN GAP ANNVILLE PA 17003-51AF	1
204 WEATHER FLIGHT 3305 FEIEBELKORN ROAD MCGUIRE AFB NJ 08641-6004	1
207 WEATHER FLIGHT 3912 W MINNESOTA ST INDIANAPOLIS IN 46241-4064	1
207 WEATHER FLIGHT 3912 W MINNESOTA ST INDIANAPOLIS IN 46241-4004	
200 M/CATTURE OF FETT 2006 A DUBLIED FINE NEW NEW AND 25 HILL-AUDIE	
208 WEATHER FLIGHT 200 AIRTORT DR ST TADE WIN 5107-4070	I
209 WEATHER FLIGHT 2210 W 35 STREET, BLDG 9 RM 119 AUSTIN TX 78703-1222 210 WEATHER FLIGHT 1280 SOUTH TOWER DRIVE ONTARIO ANGB CA 91761-7627	l

301 OD/DOBW CARSWELL ARB TX 76127-5000
304 ARRS/DOOR PORTLAND IAP OR 97218-2797
314 OSS OSW 2740 1ST ST BLDG 120 LITTLE ROCK AFB AR 72099-5060
319 OSS/OSW 695 STEEN AVE STE 106 GRAND FORKS AFB ND 58205-6244
347 OSS OSW 8227 KNIGHTS WAY STE 1062 MOODY AFB GA 31699-1899
355 OSS OSWF 4360 S PHOENIX ST BLDG 4820 DAVIS MONTHAN AFB AZ 85707-4638
366 OSS OSW 665 THUNDERBOLT ST BLDG 262 RM 11 MT HOME AFB ID 83648-5401
410 OSS OSW 401 F AVE STE 7 K I SAWYER AFB MI 49843-4010
416 OSS OSW 592 HANGAR RD BLDG 1000 STE 121 GRIFFISS AFB NY 13441-4520
482 OG/OSAW 360 CORAL SEA BLVD HOMESTEAD AFS FL 33039-1299
509 OSS OSW 745 ARNOLD AVE STE 1A WHITEMAN AFB MO 65035-5026
DET 1 549 CTS/WX 661 7TH ST BICYCLE LAKE AAF BLDG 6212 FORT IRWIN CA 92310-5000
DEL I 349 CISWA 661 / H SI BICYCLE LAKE AAF BLOG 6212 FORT IRWIN CA 92310-3000
608 COS/DOOW 245 DAVIS AVE EAST BLDG 5546 STE 245 BARKSDALE AFB LA 71110-2279
758 AS/DOV 316 DEFENSE AVE STE 101 CORAOPOLIS PA 15108-4403
901 AG/OSA USAFR (KEN GOULD) 3976 KING GRAVES RD YOUNGSTOWN/WARREN MAP VIENNA OH 44473-0910 1
AETC/XOSW 1F ST STE 2 RANDOLPH AFB TX 78150-4325
AFTT LDEE 2950 P ST BLDG 640 WRIGHT-PATTERSON AFB OH 45433-7765
AFTT CIR WRIGHT-PATTERSON AFB OH 45433-6583
AU/ACSC (MAJOR MUOLO/DEA) 225 CHENNAULT CIRCLE MAXWELL AFB AL 36112-6426
12 OSS DOW H 08, 1350 5TH ST EAST RANDOLPH AFB TX 78150-4410
14 OSS DOW 595 1ST ST STE # 3 COLUMBUS AFB MS 39710-4201
42 OS/OSWF 220 WEST ASH BLDG 844 MAXWELL AFB AL 36112-6608
45 AS/OSFWX 817 H ST STE 102 KEESLER AFB MS 39534-2452
47 OSS DOW 541 1ST ST STE 2 LAUGHLIN AFB TX 78843-5210
56 OSS/OSW 14185 WEST FALCON LUKE AFB AZ 85309-1629
OL A 58 OSS OSW BLDG 324 GILA BEND AFAF AZ 85337-5000
64 OSS DOW 145 N DAVIS DR REESE AFB TX 79489-5000
71 OSS/OSW 301 GRITZ ST STE 52 VANCE AFB 0K 73705-5412
80 OSS/DOAW 620 J AVENUE STE 3 SHEPPARD AFB TX 76311-2553
80 OSS/DOAW 620 J AVENUE SIE 3 SHEFFARD AFB 1X /0311-2333
97 OSS WXF 603 E AVE STE 1 ALTUS AFB OK 73523-5033
325 OSS OSW STOP 22 408 FLIGHTINE RD2 TYNDALL AFB FL 32403-5124
333 TCHTS TTCJB 600 FIRST STREET STE 101 KEESLER AFB MS 39534-2494
334 TRS TTMV 700 H ST BLDG 4332 KEESLER AFB MS 39534-2499
558 FTS 2065 1ST DRIVE WEST RANDOLPH AFB TX 78150-4351
NAIC TATW 4115 HEBBLE CREEK ROAD STE 33 WRIGHT-PATTERSON AFB OH 45433-5637
AFCESA WE STOP 21 TYNDALL AFR FL 32403-6001
AFMC DOW 4225 LOGISTICS AVE STE 2 WRIGHT-PATTERSON AFB OH 45433-5714
AFOTEC/WE 8500 GIBSON BLVD SE KIRTLAND AFB NM 87117-5558
AL/OEBE ARMSTRONG LABORATORY 2402 EAST DRIVE BROOKS AFB TX 78235-5114
ASC/WE BLDG 91 3RD ST WRIGHT-PATTERSON AFB OH 45433-6503
ESC ENS 5 EGLIN ST HANSCOM AFB MA 01731-2116
ESC WE 5 EGLIN ST HANSCOM AFB MA 01731-2172
256 112 6 25221 61 112 12 12 12 12 12 12 12 12 12 12 12 1
PL/GP 29 RANDOLPH ROAD HANSCOM AFB MA 01731-3010
PL/TSML 5 WRIGHT ST HANSCOM AFB MA 01731-3004
PL/GPOA (AFDIS POC) 29 RANDOLPH RD HANSCOM AFB MA 01731-3010
PL/LIAF 3550 ABERDEEN AVE SE KIRTLAND AFB NM 87117-5776
PL/LIMI 3550 ABERDEEN AVE SE KIRTLAND AFB NM 87117-5776
PL WE 3350 ABERDEEN AVENUE KIRTLAND AFB NM 87117-5776
PL WE 3350 ABERDEEN AVENUE KIKILAND AFB NM 8/11/-5//6
RL/WE 525 BROOKS RD GRIFFISS AFB NY 13441-4505
SMC SDEW 160 SKYNET ST STE 2315 LOS ANGELES CA 90245-4683
WL/DOWM 2130 8TH ST STE 11 WRIGHT PATTERSON AFB OH 45433-7552
46 OSS/OSWA 601 W CHOCTAWHATCHEE AVE STE 60 EGLIN AFB FL 32542-5719
46 TW/TSWG 211 W EGLIN BLVD STE 128 EGLIN AFB FL 32542-5429
46 TEST GROUP WE 871 DEZONIA DRIVE BLDG 1183 HOLLOMAN AFB NM 88330-7715
72 OSS OSW 3800 A AVE BLDG 240 TINKER AFB OK 73145-9108
75 OSS/OSWT 5970 SOUTHGATE DR HILL AFB UT 84056-5232
76 OSS OSW 303 LUKE DR, STE 1 KELLY AFB TX 78241-5638
77 OSS/OSW 3028 PEACEKEEPER STE 4 MCCLELLAN AFB CA 95652-1020

78 OSS/OSW 200 EAGLE ST STE 202 ROBINS AFB GA 31098-2602 1 88 OSS/OSWA 2049 MONAHAN WAY BLDG 91 WRIGHT-PATTERSON AFB OH 45433-7204 1 88 OSS/OSWB 5291 SKEEL AVENUE STE 1 WRIGHT-PATTERSON AFB OH 45433-5231 1 412 OSS/WE 85 S FLIGHTLINE RD BLDG 1200 EDWARDS AFB CA 93524-6460 1 647 SVS/SVBMA (JASON SMITH) 98 BARKSDALE ST HANSCOM AFB MA 01731-1807 1 AFSOC DOOWO 100 BARTLEY ST HURLBURT FLD FL 32544-5273 1 16 OSS/OGSW 150 BENNETT AVE BLDG 90730 HURLBURT FIELD FL 32544-5727 1 193 SOG DOW BLDG 19-101 RM 108 ASF 1 INDIANTOWN GAP ANNVILLE PA 17003-5005 1
USSPACECOM J3W 250 S PETERSON BLVD STE 116 PETERSON AFB CO 80914-3220
AMC/DOWR 402 SCOTT DR UNIT 3A1 SCOTT AFB IL 62225-5302 AMC/XOWX 402 SCOTT DR UNIT 3A1 SCOTT AFB IL 62225-5302 AMWC/WCOXI 5656 TEXAS AVENUE FT DIX NJ 08640-5000 TACC/WXF 402 SCOTT DRIVE RM 132 SCOTT AFB IL 62225-5029 15 AF DOW MARCH AFB CA 92518-5000 22 OSS OSW 53435 KANSAS CT STE 110 MCCONNELL AFB KS 67221-3720 60 OSS/OSW 401 SECOND STREET TRAVIS AFB CA 94535-5030 62 OSS/OSW 401 SECOND STREET TRAVIS AFB CA 94535-5030 62 OSS/OSW 1172 E STREET RM 127 MCCHORD AFB WA 98438-1008 89 OSS/OSW 1240 MENOHER DR BLDG 1220 ANDREWS AFB MD 20331-6511 92 OSS/OSW 901 WEST BONG STE 101 FAIRCHILD AFB WA 99011-8529 305 OSS/OSW 1730 VANDENBERG AVENUE MCGUIRE AFB NJ 08641-5509 375 OSS/OSW 433 HANGAR RD SCOTT AFB IL 62225-5029 377 ABW OTW 3400 CLARK AVE SE KIRTLAND AFB NM 87117-5776 180 OSS/OSW 301 ARIZONA AVE STE 1AF PLATTSBURGH AFB NY 12903-2705 1434 OSS/OSW 501 EAGLE WAY ST DOVER AFB DE 19902-7504 437 OSS/OSW 501 EAGLE WAY ST DOVER AFB DE 19902-7504 437 OSS/OSW 101 S BATES ST STE A BLDG 169 CHARLESTON AFB SC 29404-5013
US ATLANTIC COMMAND 1562 MITSCHER AVENUE STE 200 NORFOLK VA 23551-2488 USAFALCENT RA POPE AFB NC 28308-5000 USCENTCOM CCJ3-W BLDG 540 MACDILL AFB FL 33608-7001 USCINCPAC (J37) BOX 13 CAMP H.M. SMITH HI 96861-5025 USEUCOM J3 OD WE UNIT 30400 BOX 1000 APO AE 09128-4209 USSOCCENT SCJ2- SWO 7115 S BOUNDARY DRIVE MACDILL AFB FL 33621-5101 USSOCOM SOJ3 OW 7701 TAMPA POINT BLVD MACDILL AFB FL 33621-5323 USSOUTHCOM SWO UNIT 0640 APO AA 34001-5000 USSTRATCOM J 315 901 SAC BLVD STE 1B29 OFFUTT AFB NE 68113-6300 USSTRATCOM/J3615 901 SAC BLVD STE 1F14 OFFUTT AFB NE 68113-6700 USTRANSCOM J3/4 OW 508 SCOTT DR BLDG 1900 SCOTT AFB IL 62225-5357 USTRANSCOM J5-SC (MITRE AFDIS) 508 SCOTT DR BLDG 1900 SCOTT AFB IL 62225-5357 OL A SOCOS/WX BLDG AT 3275 BAY 50 FT BRAGG NC 28307-5203 NCDC LIBRARY FEDERAL BUILDING ASHEVILLE NC 28801-2733 NGDC/NOAA (ATTN: AF LIAISON OFFICER) MAIL CODE E/GC2 325 BROADWAY BOULDER CO 80333-3328 NIST PUBS PRODUCTION RM A635 ADMIN BLDG GAITHERSBURG MD 20899 NOAA LIBRARY-EOC4W5C4 ATTN: ACQ 6009 EXECUTIVE BLVD ROCKVILLE MD 20852

NOAA/NWS W/OMZI SSMC-Z ROOM 13148 1323 EAST-WEST HIGHWA'T SILVER SFRING IVID 20910-3203
NOAA/MASC LIBRARY MC5 325 BROADWAY BOULDER CO 80303-3328
NOAA CENTRAL LIBRARY 1315 EAST-WEST HIGHWAY STE 2000 SILVER SPRING MD 20910
NOAA/NWS W/OSD SSMC- 2 ROOM 12220 1325 EAST-WEST HIGHWAY SILVER SPRING MD 20910-3283
NWS W/OM21 1325 EAST-WEST HWY RM 13208 SILVER SPRING MD 20910
NWS W/OSD BLDG SSM C-2 EAST-WEST HWY SILVER SPRING MD 20910
NWS TRAINING CENTER 617 HARDESTY KANSAS CTTY MO 64124
DEFENSE INTELLIGENCE AGENCY DIA DIW 1B DIAC RM A4-130 WASHINGTON DC 20340-6612
DTIC-FDAC CAMERON STATION ALEXANDRIA VA 22304-6145
OFMC FEDERAL COORDINATOR FOR METEOROLOGY 8455 COLESVILLE ROAD STE 1500 SILVER SPRING MD 20910-5000 1
PACAF DOW 25 E ST STE 1232 HICKAM AFB HI 96853-5426
3 ASOS/GEW BLDG 1558 FT WAINWRIGHT AIN AK 99703-5200
3 OSS WE 7TH ST BLDG 32235 ELMENDORF AFB AK 99506-3097
DET 1 3 ASOS/GEW BLDG 1558 FT WAINWRIGHT AK 99703-5200
8 OSS WX UNIT 2139 BLDG 2858 APO AP 96264-2139
15 OSS/OSW 800 HANGAR AVE HICKAM AFB HI 96853-5244
18 OSS/OSW UNIT 5177 BOX 40 APO AP 96368-5177
25 ASOS/DOW 1102 WRIGHT AVE WHEELER AAF HI 96854-5200
OL A 25 ASOS BRADSHAW AFB HI APO AP 96556-5000
35 OSS/OSW UNIT 5011 APO AP 96319-5011
36 OSS/OSW UNIT 14035 BOX AF APO AP 96543-4035
DET 1 36 OSS/OSJ PSC 489 BOX 20 FPO AP 96536-0051
51 OSS/DOW UNIT 2051 APO AP 96278-2072
374 OSS DOW UNIT 5222 APO AP 96328-5222
OL A 374 OSS APO AP 96343-0085
OL A 3/4 OSS APO AP 90343-0083
607 WEATHER SQUADRON/DO UNIT 15173 BLDG 1506 APO AP 96205-0108
607 COS/DOW UNIT 2072 APO AP 96278-2072
OL A 607 WEATHER SQUADRON UNIT 15630 BLDG 1610 APO AP 96208-0195
OL B 607 WEATHER SQUADRON UNIT 15630 BLDG 1610 APO AP 96206-0173
OL C 607 WEATHER SQUADRON UNIT 15242 BLDG S 252 UNIT 15242 APO AP 96297-0626
OL C 607 WEATHER SQUADRON UNIT 13676 BLIO \$ 3101 RM 4 APO AP 90297-0020
DET 1 607 WEATHER SQUADRON UNIT 15674 APO AP 96258-0674
OL B DET 1 607 WEATHER SQUADRON UNIT 15118 APO AP 06224-0420
OL B DET 1 607 WEATHER SQUADRON UNIT 15118 APO AP 0624-0420
DET 2 607 WEATHER SQUADRON UNIT 15200 BLDG S 819 APO AP 96271-0136
OL A DEL 2 607 WEATHER SQUADRON UNIT 13673 APO AP 90218-0673
611 OSS/OSW 6900 9TH ST STE 205 ELMENDORF AFB AK 99506-2250
OL A DET 1 611 OSS/WE BLDG 47 432 RM 116 FT RICHARDSON AIN AK 99505-2250
354 OSS IM 1215 FLIGHT LINE AVE STE 2 EIELSON AFB AK 997026-1520
534 OSS IN 1213 PEIOTI EINE AVE STE 2 EIEESON ALB AR 37/020-1520
ARMED FORCES MEDICAL INTELLIGENCE CTR INFO SVCS DIV BLDG 1607 FT DETRICK FREDERICK MD 21702-5004 1
ARMY TRAINING AND DOCTRINE COMMAND ATDO-IW (ATTN: SWO) FT MONROE VA 23651-5000
ARMY RESEARCH LABORATORY BATTLEFIELD ENVIRONMENT DIR AMSRL-BE WHITE SANDS MISSILE RANGE NM
88002-5501
USASOC ATTN: AOIN-ST FT BRAGG NC 28307-5200
U.S. ARMY COMBAT SYS TEST ACTIVITY METEOROLOGY BRANCH, BLDG 1134 ATTN: STECS-PO-OM ABERDEEN PROVING
GRND MD 21005-5059
COMMANDER US ARMY PACIFIC (APIN-OPW) FT SHAFTER HI 96858-5100
COMMANDER, FORCES COMMAND AFIN-ICW FT MCPHERSON GA 30330-6000
DIRECTOR USA-CETEC ATTN: GL-AE FT BELVOIR VA 22060-5546
DIRECTOR, USA REDSTONE TECHNICAL TEST CENTER ATTN: STERT-TE-F-MT REDSTONE ARSENAL AL 35898-8052 1
FIRST US ARMY ATTN STAFF WEATHER OFFICER FT MEADE MD 20755-7300
SECOND US ARMY AFKD-OPI-W (AFDIS POC) FT GILLEM GA 30050-5000
HQ DA DCS OPERATIONS AND PLANS ATTN: DAMO-ZD RM 3A538, 400 ARMY PENTAGON WASHINGTON DC 20330-5000 1
HQ 629TH MI BN (CEWI), 29TH ID (LIGHT) 7100 GREENBELT ROAD GREENBELT MD 20770-3398
FIFTH U.S. ARMY AFKB-OP (SWO) FT SAM HOUSTON TX 78234-7001
SIXTH U.S. ARMY AFKC-OP-IS-SWO (AFDIS POC) PRESIDIO SAN FRANCISCO CA 94129-5000
HQ ARCENT AFRO-DSO-SWO FT MCPHERSON GA 30330-7000
LOS ALAMITOS AAF (MR ADAMS) BLDG 1 AFRC 11200 LEXINGTON DR LOS ALAMITOS CA 90720-5001
LOS ALAIVIETOS MAT (IVIK ADAIVIS) BEDO T ATRO TEXO ELATINOTON DE LOS ALAIVIETOS CA 20120-3001

NATIONAL RANGE DIRECTORATE MET BRANCH ATTN: STEWS-NR-DA-F WHITE SANDS MISSILE RANGE NM 88002-5504 1 USA DUGWAY PROVING GROUND TROPICAL TEST SITE UNIT 7140 ATTN: STEDP-MT-TM-TP APO AA 34004-5000 1

DET 5 617 WS CMR 454 UNIT 31020 APO AE 09250-0047
DET 6 617 WS UNIT 29632 APO AE 09096-5000
DET 7 617 WS UNIT 28130 APO AE 09114-5000
DET 8 617 WS UNIT 25202 HQ V CORPS G2 SWO APO AE 09079-5000
DET 9 617 WS UNIT 28216 APO AE 09173-5000
DET 10 617 WS UNIT 26410 BLDG 543 RM 111 APO AE 09182-0006
OL A DET 8 617 WS UNIT 29719 BOX 363 APO AE 09028-3728
OL A 617 WS C/O 527 MI OPS APO AE 09157-5000
OL A DET 2 617 WS CMR 438 UNIT 5240 WEATHER OFFICE APO AE 09111-5000
OL B 617 WS CMR 423 APO AE 09107-5000
OL C 617 WS CMR 445 BOX 260 APO AE 09046-5000
OL D 617 WS C/O CMR 431 APO AE 09175-6321
OL E 617 WS UNIT 31401 BOX 6 APO AE 09630-0006
CEE 017 WS CIVIL STATE BOX O'NE 0700000000
1610 ALSG(P) ATTN OIC WEATHER APO AE 09867-5000
4404 OSS/OSW ATTN AFDIS POC APO AE 09894-0408
4409 OG/WE (ATTN AFDIS POC) UNIT 66200 BOX 100 APO AE 09852-6200
4409 OCI WE (ATTN APDIS POC) UNIT 60200 BOX 100 APO AE 09832-0200
CONDIAND (FTO COOM CODE NING CONTENTIO CONTENT
COMNAVMETOCCOM CODE N312 STENNIS SPACE CTR MS 39529-5000
COMNAVMETOCCOM CODE N332 STENNIS SPACE CTR MS 39529-5001
COMNAVMETOCCOM/512 (LCDR FORD) 1020 BALCH BLVD STENNIS SPACE CENTER MS 39529-5005
COMNAVMETOCCOM (CODE N433) 1020 BALCH BLVD STENNIS SPACE CENTER MS 39529-5005
COMNAVSPECWARCOM (CODE N27 FORCE OCEANOGRAPHER) 2000 TRIDENT WAY SAN DIEGO CA 92155-5599
COMSECONDFLEET (CODE J335) FPO AE 09506-6000
COMSIXFLEET (CODE N312) CDR MCGEE FPO AE 09501-6002
FLENUMMETOCCEN ATTN: DAVE HUFF MONTEREY CA 93943-5005
FLENUMMETOCDET FEDERAL BUILDING ASHEVILLE NC 28801-2696
LIBRARIAN FLENUMMETOCEN MONTEREY CA 93943-5005
HQ USMC (CODE ASL-44/MAJOR BROWN) 2 NAVY ANNEX WASHINGTON DC 20380-1775
MARINE WING SUPPORT GROUP 27 (WO) PSC BOX 8082 CHERRY POINT MCAS NC 28532-8082
NAVAL RESEARCH LABORATORY MONTEREY CA 93943-5006
NAVAL RESEARCH LABORATORY CODE 4180 WASHINGTON DC 20375
NAVAL RESEARCH LABORATORY CODE 4180 WASHINGTON DC 20375 NAVAL RESEARCH LABORATORY CODE 4323 WASHINGTON DC 20375
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NAVAL RESEARCH LABORATORY CODE 4180 WASHINGTON DC 20375 NAVAL RESEARCH LABORATORY CODE 4323 WASHINGTON DC 20375 NAVAL POSTGRADUATE SCHOOL CODE MR/HY (ROBERT HANEY) 589 DYER RD BLDG 235 RM 2AF MONTEREY CA 93943-5114 NAVAL POSTGRADUATE SCHOOL CHMN DEPT OF METEOROLOGY CODE 63 MONTEREY CA 93943-5000 NAVAL AIR WARFARE CENTER-WEAPONS DIVISION GEOPHYSICAL SCIENCES BRANCH CODE 32AF POINT MUGU CA 93042-5001 COMMANDING OFFICER NAVEURMETOCCEN PSC 819 BOX 31 FPO AE 09645-3200
NAVAL RESEARCH LABORATORY CODE 4180 WASHINGTON DC 20375 NAVAL RESEARCH LABORATORY CODE 4323 WASHINGTON DC 20375 NAVAL POSTGRADUATE SCHOOL CODE MR/HY (ROBERT HANEY) 589 DYER RD BLDG 235 RM 2AF MONTEREY CA 93943-5114 NAVAL POSTGRADUATE SCHOOL CHMN DEPT OF METEOROLOGY CODE 63 MONTEREY CA 93943-5000 NAVAL AIR WARFARE CENTER-WEAPONS DIVISION GEOPHYSICAL SCIENCES BRANCH CODE 32AF POINT MUGU CA 93042-5001 COMMANDING OFFICER NAVEURMETOCCEN PSC 819 BOX 31 FPO AE 09645-3200 OFFICER IN CHARCE NAVEURMETOCDET PSC 817 BOX 13 FPO AE 09622-0800
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NAVAL RESEARCH LABORATORY CODE 4180 WASHINGTON DC 20375 NAVAL RESEARCH LABORATORY CODE 4323 WASHINGTON DC 20375 NAVAL POSTGRADUATE SCHOOL CODE MR/HY (ROBERT HANEY) 589 DYER RD BLDG 235 RM 2AF MONTEREY CA 93943-5114 NAVAL POSTGRADUATE SCHOOL CHMN DEPT OF METEOROLOGY CODE 63 MONTEREY CA 93943-5000 NAVAL AIR WARFARE CENTER-WEAPONS DIVISION GEOPHYSICAL SCIENCES BRANCH CODE 32AF POINT MUGU CA 93042-5001 COMMANDING OFFICER NAVEURMETOCCEN PSC 819 BOX 31 FPO AE 09645-3200 OFFICER IN CHARCE NAVEURMETOCDET PSC 817 BOX 13 FPO AE 09622-0800 OFFICER IN CHARGE NAVEURMETOCDET PSC 814 BOX 22 FPO AE 09662 OFFICER IN CHARGE NAVEURMETOCDET PSC 812 BOX 3380 FPO AE 09627-3380 NAVICECEN (LT KLEIN) 4251 SUITLAND RD FOB#4 WASHINGTON DC 20395 COMMANDING OFFICER NAVICECEN 4301 SUITLAND ROAD FOB #4 WASHINGTON DC 20395-5108 NAVLANTMETOCDET PATUXENT RIVER NAS MD 20670-5103 NAVLANTMETOCDET (AFDIS POC) PSC 1001 BOX 35-W FPO AE 09508-0014 NAVLANTMETOCEN CODE 50, ATTN: MET TEAM 931 3RD AVE MCCADY BLDG NORFOLK NAS VA 23511-2394 NAVLANTMETOCEN CODE 50, ATTN: MET TEAM 931 3RD AVE MCCADY BLDG NORFOLK NAS VA 23511-2394 NAVLANTMETOCEN CODE 9220 STENNIS SPACE CTR MS 39522-5001 NAVOCEANO CODE N25131 8100 RM 203D STENNIS SPACE CTR MS 39522-5001 NAVOCEANO CODE N25131 8100 RM 203D STENNIS SPACE CTR MS 39522-5001 NAVOCEANO CODE N25131 8100 RM 203D STENNIS SPACE CTR MS 39522-5001 NAVOCEANO CODE N25131 8100 RM 203D STENNIS SPACE CTR MS 39522-5001 NAVOCEANO CODE N25131 8100 RM 203D STENNIS SPACE CTR MS 39522-5001 NAVOCEANO CODE N25131 8100 RM 203D STENNIS SPACE CTR MS 39522-5001 NAVPACMETOCCEN WEST GUAM/ITWC PSC 489 BOX 2 FPO AP 96563-0051 NAVPACMETOCCEN ATN: TECH LIBRARY BOX 113 PEARL HARBOR HI 96860-7000 NAVPACMETOCCEN AS NORTH ISLAND SAN DIEGO CA 92135-5130
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US PACIFIC FLEET (N3WX) CSC/WILLIAM LITTLE 250 MAKALAPA DRIVE PEARL HARBOR HI 96860-7000
WEATHER SERVICE-MCAS PO BOX 55010 BEAUFORT SC 29904-5001
WEATHER SERVICE USMC (WO SMITH) MCAS BOX 555151 CAMP PENDLETON CA 92055-5151
WSO H & HS MARINE STATION WEA MCAS TUSTIN CA 92710-5000
1 MARINE EXPEDITIONARY FORCE COMMAND ELEMENT (RLO) CAMP PENDLETON CA 92055-5300
AEDC TECHNICAL LIBRARY FL2804 100 KINDEL DR STE C212 ARNOLD AFB TN 37389-3212
HUMAN RESOURCES TECHNICAL LIBRARY FL2870 AL/HR-DOKL 7909 LINDBERG DR RM 239 BLDG 578
BROOKS AFB TX 78235-5352 AFFTC TECHNICAL LIBRARY FL2806 412 TW/TSTL 307 E POPSON AVE BLDG 1400 RM 106 EDWARDS AFB
AFFTC TECHNICAL LIBRARY FL2806 412 TW/TSTL 307 E POPSON AVE BLDG 1400 RM 106 EDWARDS AFB
CA 93524-6630
TECHNICAL LIBRARY FL2825 203 W EGLIN BLVD STE 300 EGLIN AFB FL 32542-6843
ROME LAB TECHNICAL LIBRARY FL2810 RL/SUL CORRIDOR W STE 262 26 ELECTRONIC PKWY BLDG 106
GRIFFISS AFB NY 13441-4514
ROME LAB RESEARCH LIBRARY FL2807 PL/TL (LIBRARY) 5 WRIGHT ST BLDG 1103 HANSCOM AFB MA 01731-3004
TECHNICAL LIBRARY FL2051 SA-ALC/CNL 485 QUENTIN ROOSEVELT RD BLDG 171 KELLY AFB TX 782416425
PHILIPS LAB TECHNICAL LIBRARY FL2809 PL/DOSUL 3400 ABERDEEN AVE SE BLDG 419 KIRTLAND AFB NM 87117-5776
AIR UNIVERSITY LIBRARY FL3386 AUL/LD 600 CHENNAULT CIRCLE BLDG 1405 MAXWELL AFB AL 36112-6424
AUL/LSE BLDG 1405 600 CHENNAULT CIRCLE MAXWELL AFB AL 36112-6424
TECHNICAL LIBRARY FL3100 HQ SSC/RMMI 201 E MOORE DR BLDG 856 RM 1701 MAXWELL AFB
GUNTER ANNEX AL 36114-3005.
TECHNICAL LIBRARY FL2513 45-SW CSR 5123 1030 S HWY A1A BLDG 989 RM A1-S3 BOX 4127 PATRICK AFB FL
32925-0127
TECHNICAL INFO CTR FL7050 AL/EQ-TIC 139 BARNES DR STE 2 BLDG 1120 TYNDALL AFB FL 32403-5323
TECHNICAL LIBRARY FL2827 30 SPW/XPOT 806 13TH ST STE A BLDG 7015 VANDENBERG AFB CA 93437-61111
WRIGHT LAB LIBRARY FL2802 WL/DOC 2690 C ST STE 4 BLDG 22 WRIGHT-PATTERSON AFB OH 45433-7411
TECHNICAL LIBRARY FL2830 NAIC/DXLS AREA A 415 HEBBLE CREEK RD STE 9 BLDG 856
WRIGHT-PATTERSON AFB OH 45433-6508
USAFA LIBRARY FL7000 HQ USAFA/DFSEL 2354 FAIRCHILD DR STE 3A10 USAF ACADEMY CO 80840-6214